

# Neutron imaging characterization of water and heat transport in a evaporative cooled fuel cell

M. Cochet, A. Forner-Cuenca, D. Scheuble, V. Manzi-Orezzoli, J. Biesdorf, P. Boillat  
Electrochemistry Laboratory, Paul Scherrer Institut, CH-5232 Villigen, Switzerland

## Motivation

- ❖ Polymer electrolyte fuel cells (PEFC) generate electricity by converting hydrogen and oxygen into water.
- ❖ As a by-product of the chemical reaction, heat can damage the PEFC. Increased temperatures can indeed dry out the membrane and stop the reaction.
- ❖ A new concept is developed at PSI which would both cool down more efficiently, and reduce complexity and volume of the stack.<sup>1</sup>

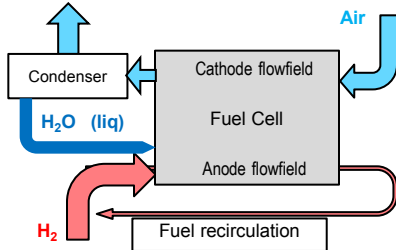


Fig 1: Principle of the evaporation cooling fuel cell stack

- ❖ Cooling is managed by bringing liquid water in the fuel cell itself through channels on the anode side, parallel to the hydrogen channels.
- ❖ Water is pumped by capillary pressure towards the membrane by modified Gas Diffusion Layers (GDL).
- ❖ Water evaporates in the cell, providing the cooling effect.

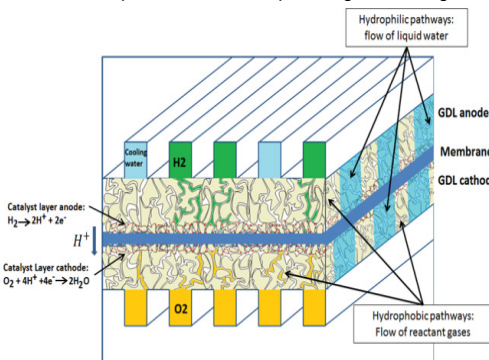


Fig 2: Water and gases transport in modified GDLs patented by PSI

- ❖ GDLs need to transport liquid water and reactant gases separately to avoid flooding.
- ❖ A synthetic method developed at PSI turns a classic GDL into a succession of hydrophobic and hydrophilic layers, defining separate pathways for gases and liquid water.<sup>1,2</sup>

## Thermal Test Cell design

- ❖ Test bench thermal boundary conditions must be representative of a fuel cell stack.
- ❖ In a fuel cell stack, between 2 cells, heat fluxes are opposite:  
$$\varphi_{anode_i - cathode_{i+1}} = -\varphi_{cathode_{i+1} - anode_i}$$
- ❖ Assuming equal temperature distributions:  
$$\varphi_{anode - cathode} = -\varphi_{cathode - anode} = -\lambda_{flowfields} \cdot \nabla T_{anode - cathode}$$
- ❖ In a classical test bench, compression body's temperature kept constant. Therefore, the heat fluxes from cell towards body not representative of stack conditions
- ❖ Measurements of the flow field's temperature ( $T_{flowfields\ anode}$  and  $T_{flowfields\ cathode}$ ) and heat fluxes  $\varphi_{flowfield - body}$
- ❖ Peltier thermoelectric coolers create heat flux in the opposite direction  $\varphi_{Peltier}$

$$\varphi_{total} = \varphi_{anode - body} - \varphi_{Peltier} = -\lambda \cdot \frac{\Delta T_{flowfields\ anode - cathode}}{\delta_{flowfield}}$$

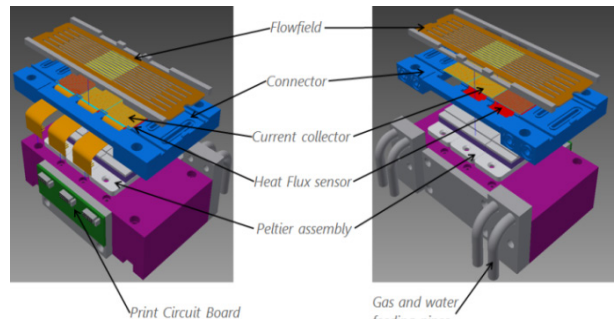


Fig 3: Design of the thermal test bench

## Pattern wettability: Neutron Radiography of a GDL

- ❖ Water was injected via a rectangular channel in perpendicular direction to the hydrophilic lines (500 μm width, spaced 1 mm).
- ❖ Capillary pressure values were set by controlling the water pressure (height of an elevated tank) and neutron radiography was performed (through-plane).
- ❖ Lateral transport of water was captured at low capillary pressure (10 mbar).
- ❖ Line width broadening was captured at higher pressures.

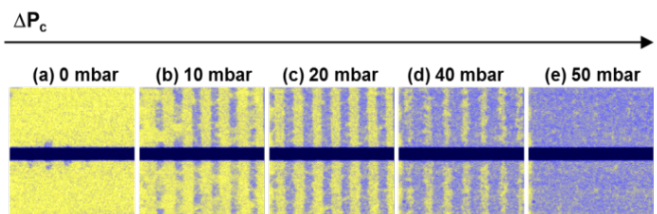


Fig 4: Water locations in the modified GDL at different capillary pressures.

## Conclusions and outlook

- ❖ A thermal test bench has been designed and built in order to prove the principle of evaporative cooling...
- ❖ Modified GDLs with patterned wettability have been developed and characterized with capillary pressure-saturation combined with neutron radiography.
- ❖ Optimization of the material synthesis and injection strategy will be carried out.

## Acknowledgement

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## References

- 1P. Boillat, et al., *European Patent Application*, EP14184065.2 (2014)
- 2A. Forner-Cuenca, et al., *Advanced Materials*, under review (2015)